

The Moon's Temperature at $\lambda=2.77\text{cm}$

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Abstract. The study of the thermal radio emission of the moon and planets began in 1946 with the detection of the thermal radiation of the moon at 1.25cm wavelength by Dicke and Beringer [1]. This was followed three years later by a comprehensive series of observations of the radiation from the moon at 1.25cm wavelength over three lunar cycles by Piddington and Minnett [2] showing that the thermal radiation from the moon at this short wavelength varied during a lunar cycle in a roughly sinusoidal fashion. The temperature, however, was much smaller than the change in the surface temperature of the moon as known from infrared observations. The maximum of radio radiation was found about 3.5 days after the maximum of the surface temperature at full moon. With the very insensitive instruments of that time it was rather difficult to measure a few Kelvin at a system temperature level of several thousand Kelvin. Now, 55 years later, I repeated such measurements with standard consumer equipment bought from the supermarket. Nowadays one can buy a complete satellite receiving system composed of a parabola mirror, a LNC (low noise converter) and a satellite receiver for the frequency range of 10.7GHz to 12.7GHz for less than 200 Swiss francs. Such a satellite system has a ~ 100 times lower system temperature than the original one of Dicke and Beringer; thus one can expect a system temperature of less than $T_{\text{sys}}=70$ Kelvins. With this paper I want to demonstrate that it is possible to repeat classical radio astronomy experiments with really cheap hardware. My own measurements over two complete cycles from 6 January until 8 March 2001 confirm within fairly large error bars the measurements of Dicke, Beringer and a few others [3, 4, 5]. I measured a mean temperature of $T_{\text{mean}}=213$ Kelvin. The minimum was about $T_{\text{min}}=192$ Kelvin $\sim 2,5$ days prior to full moon while the maximum with 236 Kelvin was about ~ 5 days after full moon.

Key words: Moon temperature, delayed maximum radiation, atmospheric absorption, system temperature, blackbody emission, geostationary satellite, noise figure.

1. Introduction

At optical wavelengths the moon and the planets are seen mainly in the sun's reflected light. Very little light is radiated from these objects acting as blackbody emitters. At radio wavelengths the situation is reversed, and the sun's reflected radiation is extremely small compared to the thermal blackbody emission. The infrared temperature is symmetrical with respect to full moon, reaching a maximum at full moon and a minimum at new moon. The microwave temperatures, on the other hand, exhibit not only a phase lag of several days, but definite asymmetry with respect to the maximum temperature.

Here I report on the observation of the moon's radiation at a wavelength of $\lambda=2.77\text{cm}$, corresponding to a microwave frequency of $f=10.83\text{GHz}$ at the lower end of the satellite Ku-communication band. It has to be checked if the radiation can be measured at all with a low cost satellite receiving equipment. In the case of a positive result it has also to be checked whether the expected phase lag of about $\Delta T=3.5$ days can be verified. Measuring methods have to be adapted or developed to measure an antenna temperature of only a few Kelvin with adequate stability and sensitivity during an observation time of at least 2 complete moon cycles. While the antenna temperature is less than 8 Kelvin, several interference sources have

to be explored and as far as possible to be taken into account within the evaluation of the final result.

2. Measuring equipment

The main part as already mentioned is a complete low cost satellite receiving system bought from a super market here in Zürich. Its low noise figure (NF) according to the specification is better than $NF=0.9\text{dB}$ (noise figure) corresponding to $T_{\text{sys}}=70$ Kelvin excess noise at room temperature. This is more than 100 times better than the receiver of Dicke and Beringer. The parabola mirror together with the LNC (low noise converter) is mounted saprophytically on the western rim of the 5m parabola antenna of the IFA (Institute of Astronomy) of ETH Zürich [3]. This mounting method allows controlling the position electronically by a standard personal computer in particular to follow the path of the moon from moon-rise to moon-set.



Fig. 1: 80cm satellite antenna mounted on a 5m dish antenna at Bleien observatory. The observatory with receiver and computers is 50m to the right side of the tower.

The personal computer can be monitored remotely and controlled via VNC (virtual network computing). Thus it is very easy to do the controlling functions in a comfortable way from my home. The computer does not only track the moon, but it also offers the method of beam-switching, a very efficient method to measure small flux changes on a warm or even hot background noise level. The LNC is powered with a bias-T, feeding $U=+15\text{Volts}$ direct current from the observatory's power supply. The frequency-depending attenuation of the 50m long cable between LNC and receiver is flattened by an ordinary TV-equaliser. The satellite IF (intermediate frequency) of 950MHz to 1.95GHz is then fed into a standard communications receiver AR5000 to select the desired receiving frequency, to amplify the noise signal and to limit the observing bandwidth to $B=220\text{KHz}$ or even less. A broader bandwidth is quite desirable, but the interference from geostationary satellite communication signals would increase drastically. The second IF of 10.7MHz is directly fed to a logarithmic detector AD8307 of Analog Devices with a conversion constant of $k=25\text{mV/dB}$. The analogue output of the logarithmic detector is directly measured with a standard bench digital multimeter FLUKE45. The RS232 output of the multimeter is fed to the communication port COM1 of an additional personal computer. It reads the serially sent data and stores them on

harddisk in ASCII format where each entry represents the radio flux expressed in volts. Subsequently the locally stored data can be transferred to my home or to the IFA via ftp.

3. Measuring methods

3.1 Frontend

It is common knowledge that the background temperature of the sky is a non-linear function of the telescopes elevation. Thus a method is needed to compensate varying background noise levels. I use a beam switching method to compensate the influences of high background noise at low elevation which is similar to the method Dicke used 55 years ago. The switching phase stays $\Delta t=90$ seconds on source, changes as fast as possible by $\Delta\alpha=6$ degrees eastward to the source for another $\Delta t=90$ seconds. This sequence is automatically repeated as long as the moon is above the horizon in Bleien. The switching time of $\Delta t=90$ second has to match with integration time and drifting variations due to temperature variations either of the LNC or of the receiver detector system. The nominal switching time has to be higher than the integration time but has also to be shorter than any drifting component in the whole system; thus in my configuration $\Delta t=90$ seconds is a good compromise. The deflection angle of $\Delta\alpha=6$ degrees is another compromise. It has to be larger than the beam angle of the telescope, but it should be as small as possible to not waste useful measuring time, because after all the antenna control system needs a couple of seconds to reach the deflection of $\Delta\alpha=6$ degrees.

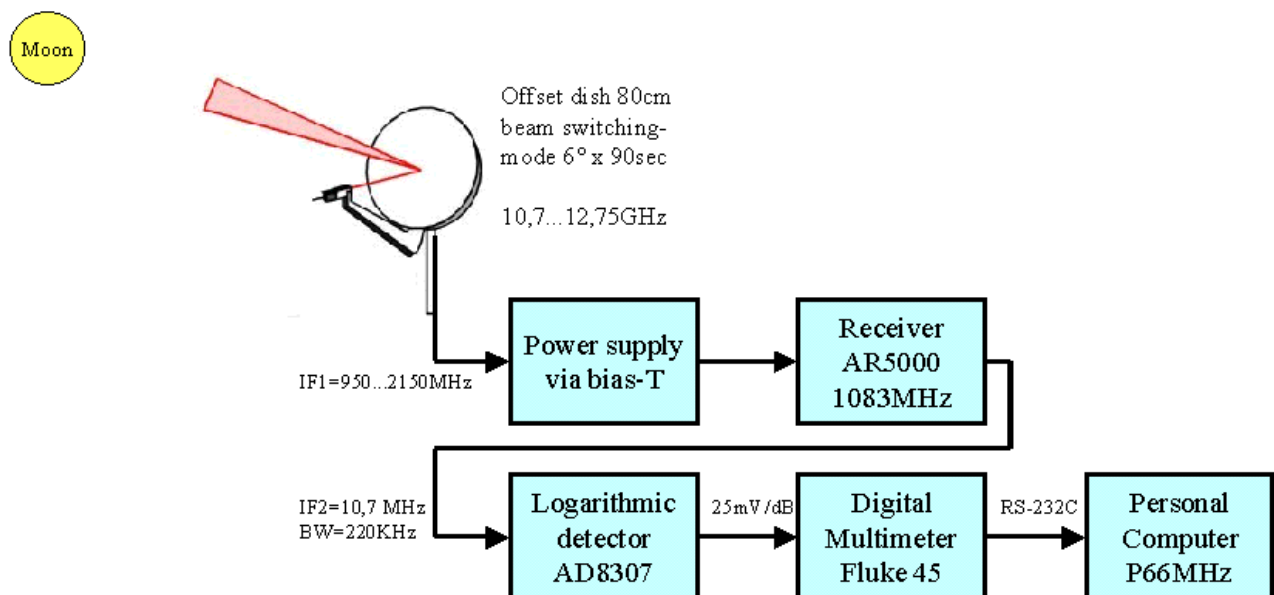


Fig. 2: Hardware structure of the radio astronomy receiving system from antennae (left) via receiver to the personal computer (right).

3.2. Backend

The collected data are visualised every day after transferring them to my home computer. The data (ASCII-files) can be visualised with EXCEL, MATH-CAD, MAT-LAB or any other spreadsheet program. Every file has to be identified with the correct starting time in UT that is

delivered through a professional GPS system from within the observatory. The data usually are split into subsequent files of 1 hour duration, 900 measurement points each, making the analysis on PC level simpler. The mean elevation ε of the telescope has to be calculated to compensate the atmospheric attenuation for every file with 1 hour duration. For correlation purposes and for visualisation processes I also need the moon phase angle ϕ , the moon disk diameter Φ and the illumination factor ξ . These values are automatically calculated by a home brewed Windows application program according to date and time UT (universal time). To calculate the antenna temperature it is necessary to know the proper reference temperature T_{ref} . In my configuration (as a first approximation) I decided to use the temperature of the logarithmic detector in the observatory $T_{ref}=T_{rx}$ (rx = receiver). This temperature can be copied free from the environmental data file `yyyymmdd.wdf` of the Phoenix-2 radiospectrograph at Bleien observatory. The datafile is stored once per day and can be viewed with any browser on <http://www.astro.phys.ethz.ch/rapp/>. The temperature T_{inc} of the LNC can also be picked out of the weather data file also with a time resolution of 1 minute.

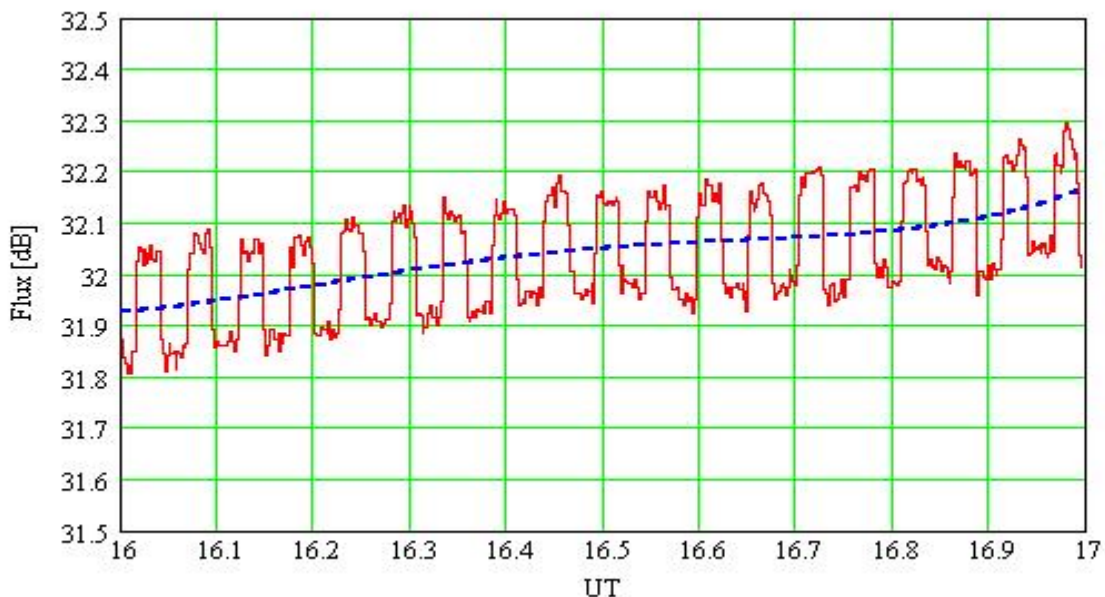


Fig. 3: Evaluation of mean moon flux in decibels using a fitting function to split background flux and moon flux. The slow variations are due to different elevation angles, temperature changes of LNC and/or changes in receiver stability. The solid red curve is subtracted from the blue dotted fitting curve. Statistical analysis (median value) of the difference pattern results in a single flux value for that file of February 16, 2001. The fitting curve is chosen in such a way that the residual dispersion or variance is a minimum. In that special case a 4th order polynom was chosen.

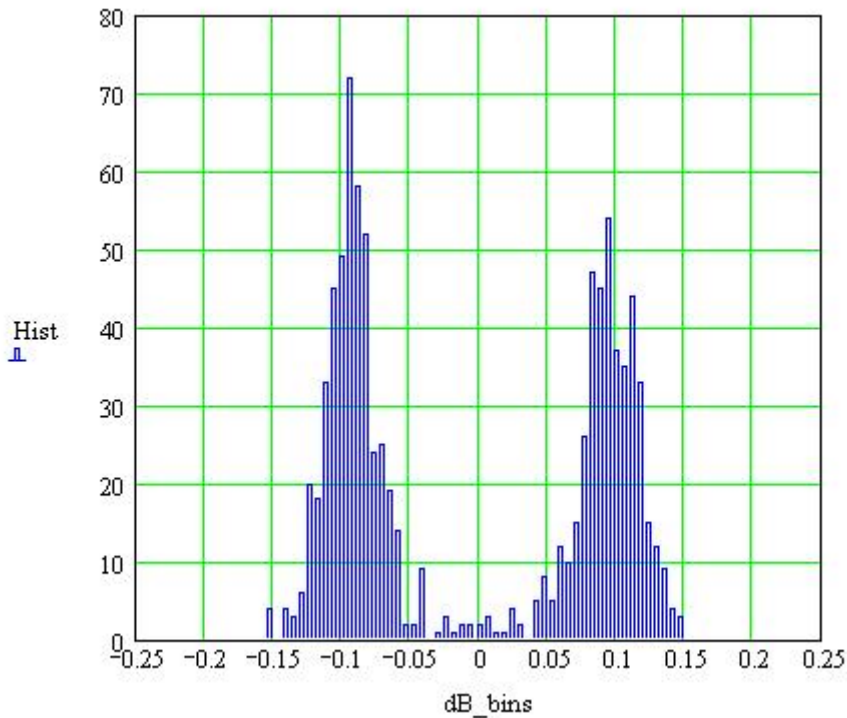


Fig. 4: Histogram of the data file of Fig. 3 above. The left peak represents the noise distribution of the background radiation only, while the right peak represents the background noise plus the excess noise distribution of the moon. The difference between both peaks is stored as a single value expressed in decibels. Here in this example, I got 0.197dB corresponding to an antenna temperature of about 4.4 Kelvin at an average system temperature of 94 Kelvin.

3.3 Analysis steps

3.3.1 Exception handling

Prior to analysis the data has to be checked for plausibility. There are a huge number of interference possibilities. All data with non-expected data were deleted, especially all with a dispersion larger than 40 Kelvin. There are several days with really exotic conditions where no useful data can be recorded. On January 15, 2001, for example, the moon was hidden by the geostationary satellite path and thus the strong radio flux saturated the receiving system; no measurement was possible. Another critical date was January 24, 2001, when the sun and moon both had similar sidereal coordinates (new moon). The sun outshines the moon several thousand times; thus no measurements were possible at all. Measurements near the horizon are often critical because of the high background temperature (300 Kelvin) or due to interference by man made noise. Another critical point was found during the experiments while using beam switching mode. Our beam switching method first worked only in horizontal (azimuthal) direction. As soon as the moon is higher than 45° above the horizon, the horizontal deflection is really unsuitable because the deflection angle on the sky is reduced due to cosine(elevation) effect. If I observed in zenith, the deflection angle would be exactly zero and we would only rotate the polarisation plane of the LNC. Therefore I introduced another option within the on/off-source method. Now I can select between horizontal or vertical deflection. Vertical deflection is not influenced by cosine(elevation) but

it is only allowed for elevations larger than 30°. Otherwise the antenna would point to the horizon every time and would therefore increase the system noise. All non-exceptional data are analyzed by the following procedures.

3.3.2 Analysis

The stored data first has to be converted into equivalent antenna temperature using an estimation of the reference temperature T_{ref} . Due to missing calibration sources, T_{ref} was calculated by three different methods. The first method uses the noise figure NF of the LNC plus internal losses of dust cover plus atmospheric attenuation plus sky background temperature which leads to about 89 Kelvin. The second method uses a back-tracking calculation of the solar radio noise measured at NOAA which leads to 90 Kelvin. And the third method uses the ambient temperature of the horizon (forest) at Bleien observatory which leads to about 104 Kelvin. I then took the average value of the above three different methods to $T_{ref} = 94$ Kelvin.

$$T_a = T_{ref} \cdot \left(10^{\frac{RFdB}{10dB}} - 1 \right) \quad (1)$$

This calculated antenna temperature is too low because of several more or less exactly known attenuation coefficients. The first not yet exactly known attenuation coefficient is the attenuation γ_c of the dust cover of the LNC. It can only be measured by killing the device. I definitely not like that method, though I took an estimation obtained from colleagues and from experience with other LNC's. One can assume that the attenuation is in the range of 0.1dB to 0.3dB, here I have decided to use 0.1dB. The end result can be corrected as soon as the dust cover can be measured.

$$\gamma_c = 10^{\frac{0.1dB}{10dB}} \quad (2)$$

Now we can calculate the antenna temperature of the moon on the earth but that's still not the proper value because the atmosphere has an attenuation of at least $aa=0.22$ dB in zenith. The value varies with different authors from 0.20dB to 0.24dB and for rainclouds even up to 1.5dB. I have decided to use the more pessimistic value of $aa=0.22$ dB. Unfortunately I never measured the moon in zenith, thus one has to take into account the non-linear increase of the attenuation for other elevations than zenith. Several papers have been published dealing this topic. The air at the horizon is thicker than in zenith thus the attenuation near the horizon is a maximum. The attenuation of the radiation due to the atmospheric absorption will decrease the measured flux of a radio source. If $S(z)$ is the flux measured at zenith distance z , and S_0 is the flux that would be obtained outside the atmosphere, then

$$S(z) = S_0 \cdot aa^{-X(z)} \quad (3)$$

where aa is the atmospheric attenuation at the zenith for the airmass 1, and $X(z)$ is the relative airmass in units of the airmass at the zenith. For a plane parallel atmospheric model clearly follows

$$X(z) = \sec(z) = \frac{1}{\cos(z)} \quad (4)$$

Schönberg 1929 [7] has done extensive investigations of $X(z)$, a Chebyshev-fit to these data up to $X=5.2$ with an error of less than 1promille is given by

$$X(z) = -0.0045 + \frac{1.00672}{\cos(z)} - \frac{0.002234}{\cos(z)^2} - \frac{0.0006247}{\cos(z)^3} \quad (5)$$

For my own calculations I decided to use the simpler version according to (4). Applied to my configuration an atmospheric correction coefficient γ_a can be calculated by

$$\gamma_a = aa^{\sin(\varepsilon \cdot \frac{\pi}{180})^{-1}} \quad (6)$$

According to Kraus [3] one has also to take into account the shape of the antenna to calculate the proper antenna temperature. Depending on form, size and shape of the antenna he proposes a shape factor κ which in my configuration is about $\kappa=1.02\pm 0.05$

All correction factors now can be combined into an overall loss factor γ .

$$\gamma = \gamma_c \cdot \gamma_a \cdot \kappa \quad (7)$$

Now we are able to calculate the proper antenna temperature T_p as a basis to estimate the final moon temperature.

$$T_p = T_a \cdot \gamma \quad (8)$$

The calculation of the moon temperature requires to know the beam geometry as exactly as possible. Several methods to evaluate the beam angle are known. I decided to measure the beam parameters by a meridian transit measurement of the sun on January 12, 2001 at a declination of $\delta=-21.6^\circ$. The normalisation and integration of the sun's transit data leads to the so-called directivity D , but unfortunately only for one polarisation. The data couldn't be integrated in a closed form thus I had to do it with the Σ -operator. First we need the radio signal of the sun not in decibels but in physical units e.g. in Kelvin antenna temperature.

$$RF = 300K \cdot \left(10^{\frac{RFdB}{10}} - 1 \right) \quad (9)$$

Then we have to normalise the antenna temperature pattern between 0 and 1.0

$$RF_n = \frac{RF - \min(RF)}{\max(RF) - \min(RF)} \quad (10)$$

The analysis of that normalized power pattern leads directly to the half power beam width HPBW

$$HPBW = 0.192h \cdot \frac{360^\circ}{24h} \cdot \cos\left(-21.6^\circ \cdot \frac{\pi}{180^\circ}\right) = 2.88^\circ \quad (11)$$

This normalised radio frequency power pattern on the other hand now can be summed up to S with

$$S = \sum_i RFn \cdot \delta\alpha \quad (12)$$

where

$$\delta\alpha = \frac{4 \text{ sec/sample}}{3600 \text{ sec/h}} \cdot \frac{360^\circ}{24h} = 0.017^\circ / \text{sample} \quad (13)$$

Now the directivity D can be quantified to

$$D = \frac{4 \cdot \pi \cdot \left(\frac{180^\circ}{\pi}\right)^2}{S^2} = 4478 \quad (14)$$

The directivity D can easily be converted into antenna gain G which can be compared with other measurement methods.

$$G = 10 \cdot \log(D) = 35.6 \text{ dB} \quad (15)$$

Again according to Kraus [3], D can directly be converted into the interesting beam solid angle Ω_a , expressed in square degrees.

$$\Omega_a = \frac{4 \cdot \pi}{D \cdot \left(\frac{\pi}{180^\circ}\right)^2} = 9.212 \quad (16)$$

On the other hand the apparent diameter Φ of the observed moon is not constant. During a moon phase angle ϕ it varies several percent. The more than three hundred individual values were calculated numerically and so the moon solid angle Ω_m expressed in square degrees can be estimated by

$$\Omega_m = \pi \cdot \left(\frac{\Phi}{2}\right)^2 \quad (17)$$

All components (1) until (17) are now known to finally calculate the moon's temperature T_m as a function of antenna temperature, system temperature, elevation, losses, beam angles and so forth.

$$T_m = T_p \cdot \frac{\Omega_a}{\Omega_m} \quad (18)$$

T_m (18) is the brightness temperature at 2.77cm wavelength averaged over the moon's disk and will be referred to as disk temperature.

4. Results

After doing all mathematics given in (1) to (18) we get a viewgraph of the moon's temperature T_m as a function of moon phase angle ϕ . The dark blue dots represent the moon temperature T_m , while the solid thick red line represents a 6th order polynomial filtered approximation of all data. The polynomial filter removes the noisy high frequency part of the curve and smoothes it. The deviation 1σ is less than 10 Kelvin ($1\sigma < 4\%$ of mean disk temperature) while the mean value is about 213 Kelvin. One can easily recognise the phase lag of the maximum temperature with 236 Kelvin of nearly 5 days after full moon and a minimum temperature of about 192 Kelvin 2 days prior to full moon.

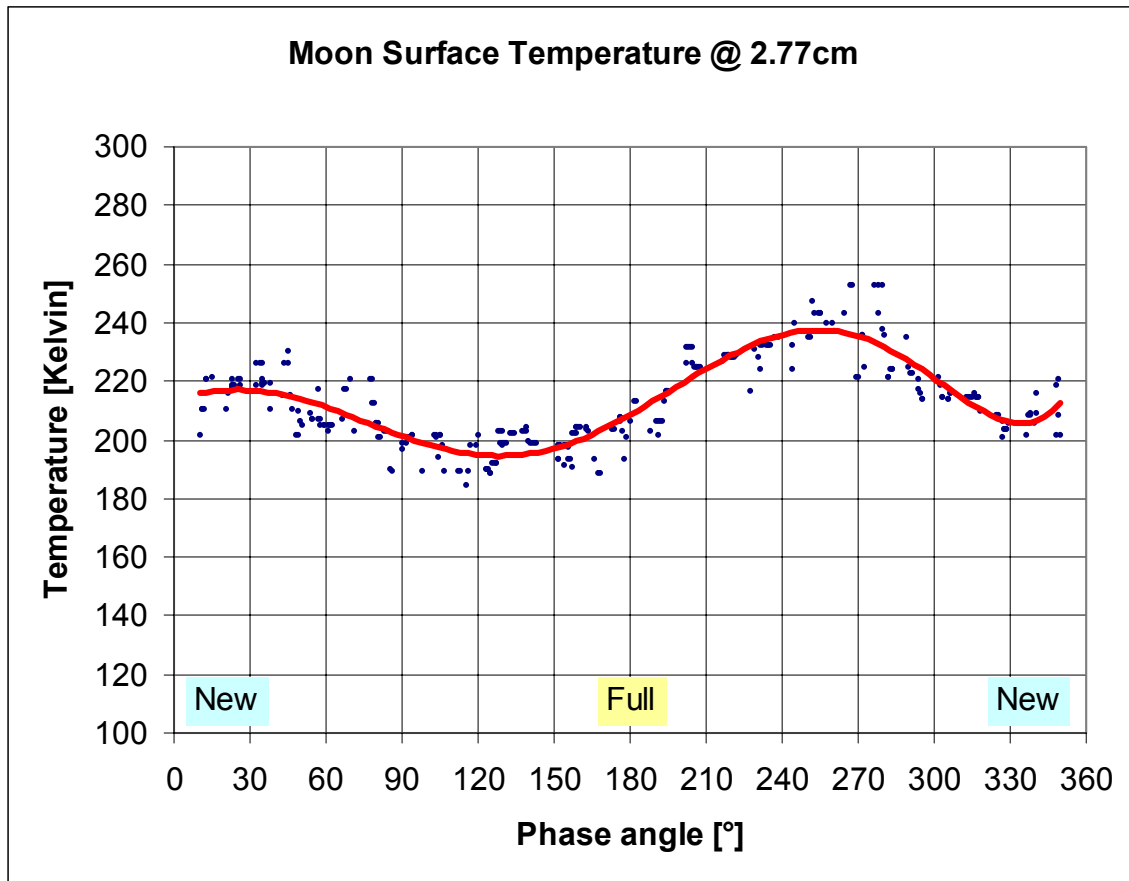


Fig. 5: Moon's disk temperature at 2.77cm wavelength versus moon phase angle ϕ during two complete cycles from twice new moon via full moon to new moon again.

5. Conclusions

I have shown that it is possible to repeat classic astronomical experiments [8] with rather simple and/or cheap hardware. Satellite LNAs nowadays have such a low system temperature that it might even be possible to detect other planets of our solar system by using adequate measuring methods, integration time and bandwidth. In the above experiment to measure the moon's disk temperature a better sensitivity could be achieved with higher integration time and/or higher bandwidth. An explanation for the higher time lag in comparison with other authors is not yet clear. Dicke and Beringer measured a time lag of about 3 | days after full moon at a wavelength of 1.25cm. In my case (5 days after full moon), I assume that at longer wavelength of 2.77cm the time lag must be larger due to the simple fact that the longer the wavelength the deeper is the penetration of the electromagnetic waves into the dust of the moon's surface. The measurement methods can be optimised using a calibrated and thermal controlled low noise converter to reduce systematically errors. An integration circuit would reduce system noise and increase the overall sensitivity drastically. Sampling data at a higher sampling rate would allow to improve statistical errors even more. More measurements should be done at the same frequency to confirm my own measurements. On the other hand, it would make sense to repeat all measurements at different frequencies to confirm the dependency of time lag on frequency. These experiments haven't been done for several years. Mankind's interest for the physical behaviour of our moon has been lost since Apollo 11, but it should be increased again. The latest paper published by Jaime Alvarez-Muñiz and Enrique Zas [9] shows that the moon comes into interest again as a very large detector for cosmic particles and neutrons. Radio observations of the whole moon may become of primary interest to physicists.

Acknowledgements. Herewith I thank Michael Arnold for upgrading the antenna control software to observe non-solar sources in on/off-source mode. I also thank Ken Becker for checking and correcting my English text. Electrical power, observation time and some network bandwidth was liberally spent by IFA ETH Zurich.

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